

**MONTHLY PROGRESS REPORT #348
FOR MARCH 2026**

EPA REGION I ADMINISTRATIVE ORDERS SDWA 1-97-1019 and 1-2000-0014

**JOINT BASE CAPE COD (JBCC)
TRAINING RANGE AND IMPACT AREA**

The following summary of progress is for the period from 01 to 31 March 2026.

1. SUMMARY OF REMEDIATION ACTIONS

Remediation Actions (RA) Underway at Camp Edwards as of 27 March 2026:

Demolition Area 1 Comprehensive Groundwater RA

The Demolition Area 1 Comprehensive Groundwater RA consists of the removal and treatment of contaminated groundwater to control further migration of explosives compounds and perchlorate. Extraction, treatment, and recharge (ETR) systems at Frank Perkins Road and Base Boundary include extraction wells, an ex-situ treatment process to remove explosives compounds and perchlorate from the groundwater, and an infiltration gallery and injection wells to return treated water to the aquifer.

The Frank Perkins Road Treatment Facility has been optimized as part of the Environmental and System Performance Monitoring (ESPM) program at Demolition Area 1. On 31 March 2025, the flow rate at the Frank Perkins Treatment Facility was reduced from 175 gallons per minute (gpm) to 100 gpm as a result of shutting down extraction well D1-EW-501, leaving only D1-EW-4 pumping as part of the Frank Perkins Road system. Due to a vault flood on 23 May 2025, which damaged electrical and pump equipment EW-501 had been operating at 100 gpm in place of EW-4. As of 27 March 2026, over 3.185 billion gallons of water were treated and re-injected. The Frank Perkins Treatment Facility was turned off on 30 September 2025 due to the government shutdown and will remain down until further notice.

The Base Boundary Mobile Treatment Unit (MTU) continues to operate at a flow rate of 65 gpm. As of 27 March 2026, over 462.2 million gallons of water were treated and re-injected. The following Base Boundary system shutdowns occurred in the reporting period:

- 0600 on 23 February 2026 due to a power interruption caused by the blizzard. The snow was cleared, and the system was restarted at 1403 on 03 March 2026.
- 1316 on 16 March 2026 due to a “Low Pressure” alarm and a VFD fault for low voltage and was restarted at 1359 on 16 March 2026.
- 0326 on 17 March 2026 due to a “Low Pressure” alarm and a VFD fault for low voltage and was restarted at 0811 on 17 March 2026.
- 0932 on 17 March 2026 due to a “Low Pressure” alarm and a VFD fault for low voltage. A faulty ice cube relay was replaced in the VDF panel, and the system was restarted at 1010 on 17 March 2026.

The Leading-Edge System was turned off with regulatory approval on 19 August 2025 (formerly operated at a flow rate of 125 gpm). Over 481.6 million gallons of water were treated and re-injected since RA.

The Pew Road MTU was turned off with regulatory approval on 08 March 2021 (formerly operated at a flow rate of 65 gpm). Over 672.9 million gallons of water were treated and re-injected during the RA.

J-2 Range Groundwater RA

Northern

The J-2 Range Northern Treatment facility consists of removal and treatment of contaminated groundwater to control further migration of explosives compounds and perchlorate. The Extraction, Treatment, and Re-infiltration system includes three extraction wells, an ex-situ treatment process to remove explosives compounds and perchlorate from the groundwater, and infiltration galleries to return treated water to the aquifer.

The Northern MTUs E and F continue to operate at a flow rate of 250 gpm. As of 27 March 2026, over 2.435 billion gallons of water have been treated and re-injected. The following MTU E and F system shutdowns occurred in the reporting period:

- 0600 on 23 February 2026 due to a power interruption caused by the blizzard. The snow was cleared, and the system was restarted at 0922 on 04 March 2026.

The Northern Treatment Building G continues to operate at a flow rate of 225 gpm. As of 27 March 2026, over 1.868 billion gallons of water have been treated and re-injected. The following MTU G system shutdowns occurred in the reporting period:

- Between 31 January and 01 February 2026 due to a phase loss caused by a blown fuse on a utility pole. The system will remain off until repairs are made.

Eastern

The J-2 Range Eastern Treatment system consists of removal and treatment of groundwater to minimize downgradient migration of explosives compounds and perchlorate. The ETI system includes the following components: two extraction wells, an ex-situ treatment process consisting of an ion exchange (IX) resin and granular activated carbon (GAC) media to treat perchlorate and explosives compounds, and two infiltration galleries. The flow rate at MTU J was reduced from 120 gpm to 90 gpm and MTU K was turned off with regulatory approval on 28 October 2025. The J-2 Range Eastern system has been running at a combined total flow rate of 340 gpm.

The MTUs H and I have been operating at a flow rate of 250 gpm. As of 27 March 2026, over 2.047 billion gallons of water have been treated and re-injected. The following MTUs H and I shutdowns occurred in the reporting period:

- 0650 on 19 December 2025 to prevent damage to the system due to a broken insulator and a blown fuse caused by high winds. MTUs H and I will remain off until further notice.

MTU J has been operating at a flow rate of 90 gpm. As of 27 March 2026, over 959.5 million gallons of water have been treated and re-injected. The following MTU J shutdowns occurred in the reporting period:

- 0650 on 19 December 2025 to prevent damage to the system due to a broken insulator and a blown fuse caused by high winds. MTU J will remain off until further notice.

MTU K was turned off with regulatory approval on 28 October 2025. (formerly operated at a flow rate of 125 gpm). Over 1.086 billion gallons of water were treated and re-injected during the RA.

J-3 Range Groundwater RA

The J-3 Range Groundwater RA consists of removal and treatment of contaminated groundwater to control further migration of explosives compounds and perchlorate. The ETR system includes four extraction wells, an ex-situ treatment process to remove explosives compounds and perchlorate from the groundwater and utilizes the existing Fuel Spill-12 (FS-12) injection wells to return treated water to the aquifer.

The J-3 system is currently operating at a flow rate of 255 gpm. As of 27 March 2026, over 2.059 billion gallons of water have been treated and re-injected. The following J-3 system shutdowns occurred in the reporting period:

- 0356 on 23 February 2026 due to a power interruption caused by the blizzard. The snow was cleared, and the system was restarted at 0837 on 02 March 2026.
- 1843 on 24 March 2026 due to an “Effluent Tank High” alarm due to FS-12 being off and was restarted at 0859 on 25 March 2026

J-1 Range Groundwater RA

Southern

The J-1 Range Southern Groundwater RA consists of removal and treatment of contaminated groundwater to control further migration of explosives compounds. The ETR system includes one extraction well, an ex-situ treatment process to remove explosives compounds from the groundwater, and an infiltration gallery to return treated water to the aquifer.

The Southern MTU has been optimized as part of the ESPM program at J-1 Range Southern. The on-base extraction well J1SEW0001 was turned off with regulatory approval on 28 February 2017 (formerly operated at a flow of 35 gpm), and flow was increased from 90 gpm to 125 gpm at the Leading-Edge extraction well J1SEW0002. The Leading-Edge extraction well has been operating at a flow rate of 125 gpm. As of 27 March 2026, over 899.5 million gallons of water have been treated and re-injected. The following shutdowns occurred in the reporting period:

- 0650 on 19 December 2025 to prevent damage to the system due to a broken insulator and a blown fuse caused by high winds. J-1 Southern MTU will remain off until further notice.

Northern

The J-1 Range Northern Groundwater RA consists of removal and treatment of contaminated groundwater to control further migration of explosives compounds and perchlorate. The ETR system includes two extraction wells, an ex-situ treatment process to remove explosives compounds and perchlorate from the groundwater, and an infiltration gallery to return treated water to the aquifer.

The Northern MTU continues to operate at a total system flow rate of 250 gpm. The flow rates for the two extraction wells at J-1 Northern were modified on 28 October 2024 based on regulatory agency concurrence with the J-1 Range Northern Data Presentation for January

2023 to December 2023. The flow rate at J1NEW0001 was reduced from 125 gpm to 85 gpm and the flow rate at J1NEW0002 was increased from 125 gpm to 165 gpm.

As of 27 March 2026, over 1.594 billion gallons of water have been treated and re-injected. The following J-1 Range Northern MTU shutdowns occurred in the reporting period:

- The system is estimated to have shut down on 23 February 2026 due to a power interruption caused by the blizzard. It is estimated that the system automatically restarted 02 March 2026 after approximately 179 hours of downtime.

Central Impact Area RA

The Central Impact Area (CIA) Groundwater treatment system consists of removal and treatment of groundwater to minimize downgradient migration of explosives compounds and perchlorate. The ETR system includes the following components: three extraction wells, an ex-situ treatment process consisting of an ion exchange resin and granular activated carbon media to treat explosives compounds, and three infiltration galleries to return treated water to the aquifer. CIA systems 1, 2 and 3 continue to run at a total flow rate of 750 gpm. As of 27 March 2026, over 4.299 billion gallons of water have been treated and re-injected. The following CIA shutdowns occurred in the reporting period:

- 0521 on 23 February 2026 CIA-1 tripped due to a power interruption caused by the blizzard and was restarted at 1836 on 27 February 2026 after power was restored.
- 0521 on 23 February 2026 CIA-2 tripped due to a power interruption caused by the blizzard and was restarted at 1836 on 27 February 2026 after power was restored.
- 0600 on 23 February 2026 CIA-3 due to a power interruption caused by the blizzard. The snow was cleared, and the system was restarted at 0953 on 03 March 2026.
- 0206 on 04 March 2026 CIA-2 tripped due to a "Floor Sump" alarm caused by a broken hose on the GAC#5 effluent. A new flange, camlock fitting, and hose were installed and CIA-2 was restarted at 0850 on 04 March 2026.
- 0541 on 19 March 2026 CIA-1 tripped due to a power interruption and was restarted at 0719 on 19 March 2026.
- 0541 on 19 March 2026 CIA-1 tripped due to a power interruption and was restarted at 0822 on 19 March 2026.

2. SUMMARY OF ACTIONS TAKEN

Operable Unit (OU) Activity as of 27 March 2026:

CIA

- Source Area Investigation
 - Conducted routine visual inspections of the consolidated shot structure (CSS) cover and surface area around the perimeter of the CSS.
- Annual sampling within the CIA SPM Program

Demolition Area 1

- No activity

Demolition Area 2

- No activity

J-1 Range

- Bag filters changed at the J-1 Range Northern system on 13 March 2026

J-2 Range

- No activity

J-3 Range

- No activity

L Range

- No activity

Small Arms Ranges

- No activity

Northwest Corner

- No activity

Training Areas

- No activity

Impact Area Roads

- No activity

Sierra Range

- No activity

Other

- Collected process water samples from Central Impact Area, Demolition Area 1, J-1 Range Northern, J-2 Range Northern, and J-3 Range treatment systems. No samples were collected from J-1 Range Southern and J-2 Range Eastern, as these systems were offline.

JBCC Impact Area Groundwater Study Program (IAGWSP) Tech Update Meeting Minutes for 08 January 2026**Project and Fieldwork Update**

Darrin Smith (USACE) provided the project and fieldwork update. The Central Impact Area (CIA) annual groundwater sampling event is ongoing and will likely run through the end of March. After that is completed, the Demolition Area 1 (Demo 1) annual groundwater sampling event will begin. The March operations and maintenance (O&M) sampling was completed on March 11, 2026 and results are pending. The February O&M sampling results indicated that CIA-2 midfluent concentrations are now below the respective action levels of 0.25 micrograms per liter ($\mu\text{g/L}$) for RDX and above the 0.35 $\mu\text{g/L}$ action level for perchlorate with a result of 0.37 $\mu\text{g/L}$. Associated media changeouts are planned. Treatment systems at Demo 1 Frank Perkins Road, J-1 South, J-2 East (H, I, and J) were offline in January and February. All systems that

were not already offline, went offline on February 23, 2026 due to the blizzard. Those systems were restarted on March 3, 2026. J-1 South, J-2 East (H, I, and J), J-2 North (G) were offline before the blizzard and remain offline due to power line damage from a previous storm, which occurred prior to the blizzard. Demo 1 Frank Perkins Road was shut off September 30, 2025 due to the government shutdown and it remains offline.

Len Pinaud (MassDEP) asked why it is taking so long for power line repairs for treatment systems that have been off since December. Shawn Cody (IAGWSP) responded that there was a delay in repairs due to lack of “new year” funding, which was needed due to the unexpected power line damage. Mr. Cody (IAGWSP) noted that after the necessary funding was released, the blizzard happened. The work is now being contracted.

Document and Project Tracking

Jeff Dvorak (USACE) reviewed the tracking list for documents and upcoming presentations.

J-2 Range Northern 2025 Annual Environmental Monitoring Report (EMR) Presentation

Ryan Hupfer (USACE) began his presentation on the J-2 Range Northern (J-2 N) Annual 2024 Environmental Monitoring Report, which covers the reporting period of November 1, 2024, through October 31, 2025. He displayed a figure showing the J-2 N operable unit and the current depictions of the extent of the current RDX and perchlorate plumes at the site. He pointed out the three extraction wells that are part of the extraction, treatment, and reinfiltration (ETR) system (EW0001, EW0002, and EW0003).

Mr. Hupfer (USACE) displayed a figure showing the RDX plume extent to the 0.97 µg/L risk-based concentration (RBC) and the remaining extent of the perchlorate plume to the 2 µg/L Massachusetts Maximum Contaminant Level (MMCL). He noted that the site has been divided into three zones: Zone 1 upgradient of EW0001, Zone 2 extending from EW0001 to past EW0002 moving to the northeast, and Zone 3 extending from just downgradient of EW0002 to EW0003. He explained that the ETR system has two different facilities to treat the water that's being extracted. Modular treatment units (MTUs) E and F are located between EW0001 and EW0002 to treat the groundwater extracted from EW0001 and EW0002. He added that treatment facility G is located close to EW0002, in Zone 3, and that treats the water from EW0003.

Mr. Hupfer (USACE) reviewed the system metrics including the percentage of the time that the system was operable during reporting period and any downtime for various reasons, which can include power outages, maintenance, mechanical and/or electrical issues, etc. He stated that MTUs E and F had a combined system uptime of 99% during the reporting period and treatment facility G had an uptime of 67%. Mr. Hupfer (USACE) noted facility G had unusually long periods of downtime between March and July and September 2025. Between March and July 2025, the system was shut down due to reduced pumping rate and grinding noises (i.e., indicators of pump failure). The pump and motor were replaced on July 01, 2026. In September 2025 there was a broken check valve on the influent line. A new check valve was installed on September 23, 2025.

Mr. Hupfer (USACE) reported on the trends in influent concentrations and mass removal for the two treatment facilities. During the current reporting period, perchlorate concentrations at MTUs E and F ranged from 0.9 to 1.4 µg/L, RDX concentrations were non-detect (ND), and HMX was

ND to below the 2 µg/L reporting limit. Mr. Hupfer (USACE) noted that the figure also shows the outline for the perchlorate MMCL of 2 µg/L.

Mr. Hupfer (USACE) also reviewed the contaminant mass removal and the cumulative contaminant mass removal throughout the operation of the systems. There were no changeouts during the reporting period of the ion exchange resin (IX) or the granular activated carbon (GAC) in the systems. For contaminant mass removal since system startup, ~120 lbs of perchlorate have been removed and very little RDX and HMX in comparison. During the reporting period, MTUs E and F removed 1.31 lbs of perchlorate, no RDX, and a trace amount of HMX.

Mr. Hupfer (USACE) stressed that there were different scales on the plots between MTUs E and F vs. treatment facility G. For MTUs E and F, the scales on the plots ranged from 0 to about 120 lbs. The scale on the plots for treatment facility G, ranged from 0 to 10 lbs. He reiterated that concentrations at treatment facility G have historically been significantly lower compared to MTUs E and F. Concentrations at facility G have been well below the RDX RBC since system operations started. Concentrations of perchlorate continue to trend downwards and leveled off over the past few years. The highest concentration of perchlorate was 0.2 µg/L during the reporting period. RDX and HMX were ND during the reporting period.

Mr. Hupfer (USACE) reviewed the cumulative contaminant mass removal trends for facility G, reiterating the scales were 0 to 10 lbs. For contaminant mass removal since system startup, ~9 lbs of perchlorate have been removed and very little RDX and HMX in comparison. During the reporting period, facility G removed 0.1 lbs of perchlorate and no RDX. There were no changeouts during the reporting period of the IX or GAC in the systems.

A map of the perchlorate monitoring network and the concentrations during the reporting period was displayed. The results were as follows: 47 well screens were sampled for perchlorate with concentrations ranging from ND to 6.6 µg/L (MW-587M1). Four screens had exceedances greater than the 2 µg/L MMCL and no screens exceeded the 15.0 µg/L health advisory (HA). The trends indicate the perchlorate concentrations at the site are trending downwards.

Mr. Hupfer (USACE) restated that the only area of the site with a perchlorate plume is Zone 2, which is in the middle of the operable unit. MW-587 defines the plume since it is the only well currently with an exceedance. Mr. Hupfer (USACE) reviewed the perchlorate trend plots noting the four wells with exceedances (MW-348M2, MW-587 M1 and M2 and EW0002) and emphasizing how contaminant concentrations are moving across the site. He explained that concentrations were once at 60 µg/L at MW-348M2 in the early 2000s and then there was a pretty sharp drop off. He noted concentrations have been consistently below the MMCL and only a brief period above it. He noted that during the reporting period, the concentrations were below the MMCL.

Mr. Hupfer (USACE) highlighted well MW-587 M1, noting it was ND in 2010s and then there was an uptick up to ~30 µg/L in 2020s. However, since that time, concentrations have dropped significantly to the 5-10 µg/L range and are currently trending downward. This indicates groundwater is moving through the area and towards the extraction well. He noted that there is a similar pattern at MW-587 M2. He also noted an increase and an exceedance at MW-703 M1. This well had not had an exceedance before the reporting period. Concentrations have gradually increased over the last few years. A plume has been delineated with very limited extent based on the exceedance. It will be monitored over the next few years.

Mr. Hupfer (USACE) displayed a longitudinal cross section of the perchlorate plume along the A-A prime that bisects the site. The cross section also shows the vertical capture zones for the three extraction wells. He stated it is important to note the vertical location of the perchlorate plume, which is well within the vertical capture zone of EW0002. He stated that the extraction well is operating as intended.

A map of the RDX monitoring network and the concentrations during the reporting period was displayed. The results were as follows: 10 well screens were sampled for RDX and concentrations ranged from ND to 1.2 µg/L (MW-585 M3). This is the only well screen with exceedance greater than the 0.97 µg/L RSL and no wells exceeded the 2 µg/L HA. Mr. Hupfer (USACE) showed the trend plots for MW-585 M3. He noted that there had been exceedances of the RSL historically at MW-289 M2, but that is no longer the case.

He commented that the RDX plume is narrow and small, compared to the size of the operable unit, and it's confined to Zone 1. Mr. Hupfer (USACE) showed the longitudinal cross section along the A-A prime line for the RDX plume at 0.97 µg/L. He said he is expecting attenuating concentrations below the RSL in the near future.

Mr. Hupfer (USACE) presented information on the aquifer hydraulic analyses that were performed using data collected during the reporting period. In October 2025 there was a synoptic water level gauging event performed. The water levels measured during the recording period range from 67.45 feet above the main sea level (MSL) measured at MW-164 M1 to the lowest groundwater elevation measured was 56.59 feet at MW-55. The horizontal gradient was calculated using those elevations and was 0.00112 feet per feet, which is in line with previous years.

Mr. Hupfer (USACE) reviewed the modeling that was performed using the 2025 pumping rates and presented the capture zones for the three extraction wells and Zone 2, which includes Water Supply (WS) Wells 1, 2, and 3. Mr. Hupfer (USACE) highlighted the lateral extent of the capture zone and the lateral extent of the plumes.

The observed perchlorate concentrations and the model-predicted perchlorate concentrations were presented. The concentrations match up closely with just a slight difference upgradient extent of the MW-587 M1 plume. He noted these are relatively new concentrations and had not yet been incorporated into the plume shell. A plume shell update is planned in the near future.

Mr. Hupfer (USACE) reviewed the observed and model-predicted perchlorate concentrations for the extraction wells. He also reviewed the observed and model-predicted perchlorate mass removal at MTU E and F and treatment facility G.

Mr. Hupfer (USACE) reviewed the Decision Document (DD) dates for each zone with model-predicted perchlorate influent concentrations for the site from 2008, through the reporting period, and out to 2030. He also reviewed the observed concentrations for each zone to date. For Zone 1 and 3, perchlorate has been cleaned up, which is in line with the DD model-predicted cleanup time of 2026 for Zone 1 and 2023 for Zone 3. The last remaining zone with exceedances of the perchlorate MMCL is Zone 2. The model-predicted cleanup was 2027 but the updated 2025 model-predicted cleanup time is 2034 due to lingering perchlorate concentrations previously mentioned.

The IAGWSP has three recommendations for treatment system operations and extraction rates for the extraction wells. The first recommendation is to shut down J-2 EW-3 and treatment facility G. Second, increase the pumping rate at EW-2 from 100 to 125 gallons per minute (gpm). Finally, reduce the pumping rate at EW-1 from 150 to 125 gpm. If the recommended optimizations are approved, IAGWSP proposes to also add five wells to the perchlorate monitoring program in and downgradient of Zone 3. There are no suggested changes to the hydraulic monitoring program.

The rationale for these recommendations is due to Zone 3 perchlorate concentrations consistently below the MMCL. The long-term trends in influent concentrations and mass removal indicate that the system is no longer actively removing appreciable quantities of perchlorate mass from the aquifer. The increase the pumping rate at J2EW0002 from 100 gpm to 125 gpm will expand the capture zone, which would prevent downgradient migration of the isolated plumelets on the margins of the current capture zone for Zone 2.

This could increase perchlorate mass removal rate since perchlorate at J2EW0002 (2.4 µg/L) is greater than at J2EW0001 (0.46 µg/L). The highest flow rate at which this well can be operated is with the current piping configuration at MTUs E&F. A decrease of the pumping rate at J2EW0001, from 150 gpm to 125 gpm, is necessary to accommodate the increase at J2EW0002.

Mr. Hupfer (USACE) explained that there is rationale for shutting down system G because the system has removed 9.35 lbs. of perchlorate (and 0.02 lbs. of RDX) since system startup in August 2006. The system removed 8.40 lbs. (~90%) of perchlorate from startup to October 2020. The rate of perchlorate mass removal has been decreasing, and the system is no longer removing appreciable mass.

Mr. Hupfer (USACE) showed figures representing the predicted effects of recommended optimizations at EW-1. The predicted changes to lateral capture zone after reducing the pumping rate from 150 gpm to 125 gpm show a reduction of ~50 feet in the area of the RDX plume (between the MW-289 and MW-585 clusters) and in the area downgradient of EW-1. Wells with RDX exceedances remain within the lateral extent of the capture zone. The predicted changes to lateral capture zone after increasing EW-1 from 100 gpm to 125 gpm are largely unchanged upgradient (i.e., southwest) of EW-1. There is marginal expansion (i.e., 50 feet or less) in the areas immediately side gradient and downgradient of EW-2. Wells with perchlorate exceedances remain within the lateral extent of the capture zone of EW-2. Mr. Hupfer (USACE) noted that the predicted effects of the optimizations on mass removal are negligible at a lower pumping rate since there are no perchlorate plumes present upgradient. There is more mass removal at the higher pumping rate; however, there is a marginal increase due to the relatively small mass of perchlorate remaining at the site.

In summary, Mr. Hupfer (USACE) reviewed the IAGWSP recommendations: Turn off EW-3 and cease operations at treatment facility G, decrease the pumping rate at EW-1 from 150 gpm to 125 gpm, increase the pumping rate at EW-2 from 100 gpm to 125 gpm, and add monitoring wells to the perchlorate monitoring program in and downgradient of Zone 3 to monitor for perchlorate downgradient of EW-2. He reiterated the benefits include expanding the capture zone at EW-2 to further prevent downgradient migration of perchlorate and the perchlorate and RDX plumes remain in the capture zones of the remaining extraction wells.

Mr. Pinaud (MassDEP) pointed out that there are two public water supply wells downgradient of the plume and just north of Gibbs Road. Mr. Pinaud (MassDEP) asked for clarification of the

locations of the five additional wells that are being proposed for monitoring as part of the optimization. Mr. Hupfer (USACE) showed a figure with a wider view and pointed out the proposed locations. Mr. Hupfer (USACE) clarified that the recommendation would add five existing monitoring wells back into the monitoring network and no new wells would need to be drilled. Mr. Pinaud (MassDEP) asked for confirmation that these wells are screened appropriately and Mr. Hupfer (USACE) confirmed that was the case. Mr. Pinaud (MassDEP) referenced a well fence farther out and asked if those screens had been evaluated for downgradient monitoring. Mr. Hupfer (USACE) said those wells had not been looked at for this optimization effort. Mr. Pinaud (MassDEP) mentioned that there were also sentry wells in the vicinity for the public water supply wells, and he believes those are being monitored by the Upper Cape Regional Water Supply Cooperative. Mr. Pinaud (MassDEP) said he wants to be sure there is appropriate monitoring if an extraction well is going to be shut down near public water supply wells. Mr. Pinaud (MassDEP) asked that the report includes the details about the additional monitoring wells. Mr. Hupfer (USACE) replied that he would confirm that information is included in the report. Jessica Crispin (MassDEP) also asked for clarification about the frequency of the sampling events and an estimate of the travel times. Mr. Hupfer (USACE) noted the five additional wells would be sampled biennially. He will review the travel times more closely, but he recalled it was approximately one mile away.

At the conclusion of the meeting, Ms. Cutler (IAGWSP) noted that the next Joint Base Cape Cod Cleanup Team meeting will be held on Wednesday, March 25, 2026 at 6PM. She offered to add people to the distribution list if they had not received a prior meeting invitation and would like to receive meeting information in the future.

Next Tech Meeting: April 9, 2026

JBCC Cleanup Team Meeting

The next JBCC Cleanup Team (JBCCCT) meeting is scheduled for 27 May 2026. Meeting details and presentation materials from previous meetings can be found on the IAGWSP web site at <http://jbcc-iagwsp.org/community/impact/presentations/>. The Cleanup Team meeting discusses late breaking news and responses to action items, as well as updates from the IAGWSP and the Installation Restoration Program (IRP). The JBCCCT meetings provide a forum for community input regarding issues related to both the IRP and the IAGWSP.

3. SUMMARY OF DATA RECEIVED

Table 1 summarizes sampling for all media from 01 to 31 March 2026. Table 2 summarizes the validated detections of explosives compounds and perchlorate for all groundwater results received from 01 to 31 March 2026. These results are compared to the Maximum Contaminant Levels/Health Advisory (MCL/HA) values for respective analytes. Explosives and perchlorate are the primary contaminants of concern (COC) at Camp Edwards. Table 3 summarizes the validated detections of per- and polyfluoroalkyl substances (PFAS) for influent and groundwater results analyzed by EPA draft Method 1633 and received from 01 to 28 March 2026. Table 3 PFAS results are compared to the Regional Screening Levels (RSLs) published by EPA in November 2023. No PFAS validation was completed during March 2026, therefore, Table 3 is not included.

The operable units (OUs) under investigation and cleanup at Camp Edwards are the Central Impact Area, Demolition Area 1, Demolition Area 2, J-1 Range, J-2 Range, J-3 Range, L Range, and Small Arms Ranges. Environmental monitoring reports for each OU are generated each year to evaluate the current year groundwater results. These reports are available on the site Environmental Data Management System (EDMS) and at the project document repository (IAGWSP office).

4. SUBMITTED DELIVERABLES

Deliverables submitted during the reporting period include the following:

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|---|---------------|
| • Response to Comments on the Draft Final Northwest Corner Demonstration of Compliance Report | 06 March 2026 |
| • Draft J-2 Range Eastern EMR for November 2024 through October 2025 | 13 March 2026 |
| • Project Note: Small Arms Ranges Operable Unit Post-Decision Document Completion of Work | 17 March 2026 |
| • Final Demolition Area 2 Demonstration of Compliance Report | 21 March 2026 |
| • Draft J-2 Range Northern EMR for November 2024 through October 2025 | 23 March 2026 |
| • Response to Comments on the Draft Demolition Area 1 EMR for July 2024 through June 2025 | 24 March 2026 |
| • Final Northwest Corner Demonstration of Compliance Report | 26 March 2026 |
| • Draft J-1 Range Northern EMR for January 2024 through December 2025 | 26 March 2026 |
| • Draft Land Use Controls Monitoring Report for 2025 | 30 March 2026 |

5. SCHEDULED ACTIONS

The following actions and/or documents are being prepared in March 2026.

- Response to Comments on the Draft J-3 Range EMR for September 2023 through August 2024
- Response to the Comments on the Draft L Range Environmental Monitoring Report for March 2024 through February 2025
- Response to Comments on the Draft J-1 Range Southern EMR for January 2024 through December 2024
- Response to Comment on the CIA EMR for July 2024 through June 2025
- Response to Comments on the IAGWSP Comprehensive PFAS Report
- Draft Site-Wide QAPP Update
- Final Demolition Area 1 EMR for July 2024 through June 2025

TABLE 1
Sampling Progress: March 2026

Area Of Concern	Location	Field Sample ID	Sample Type	Date Sampled	Matrix	Top of Screen (ft bgs)	Bottom of Screen (ft bgs)
Central Impact Area	MW-96M2	MW-96M2_S26	N	03/30/2026	Ground Water	160.00	170.00
Central Impact Area	MW-96M1	MW-96M1_S26	N	03/30/2026	Ground Water	206.00	216.00
Central Impact Area	MW-95M1	MW-95M1_S26	N	03/30/2026	Ground Water	202.00	212.00
Central Impact Area	MW-86S	MW-86S_S26	N	03/30/2026	Ground Water	143.00	153.00
Central Impact Area	MW-86M2	MW-86M2_S26	N	03/30/2026	Ground Water	158.00	168.00
Central Impact Area	MW-441M2	MW-441M2_S26	N	03/25/2026	Ground Water	109.45	119.45
Central Impact Area	MW-441M1	MW-441M1_S26	N	03/25/2026	Ground Water	204.63	214.63
Central Impact Area	MW-338M1	MW-338M1_S26	N	03/25/2026	Ground Water	189.00	199.00
Northwest Corner	MW-338M1	MW-338M1_S26	N	03/25/2026	Ground Water	189.00	199.00
Central Impact Area	MW-628M1	MW-628M1_S26	N	03/25/2026	Ground Water	230.80	240.80
Central Impact Area	MW-617M1	MW-617M1_S26	N	03/25/2026	Ground Water	175.80	185.80
Central Impact Area	MW-180M3	MW-180M3_S26	N	03/24/2026	Ground Water	171.00	181.00
Central Impact Area	MW-626M2	MW-626M2_S26	N	03/24/2026	Ground Water	237.20	247.20
Central Impact Area	MW-607M3	MW-607M3_S26	N	03/24/2026	Ground Water	157.40	167.40
Central Impact Area	MW-607M2	MW-607M2_S26	N	03/24/2026	Ground Water	177.40	187.40
Central Impact Area	MW-607M1	MW-607M1_S26	N	03/24/2026	Ground Water	207.40	217.40
Central Impact Area	MW-607M1	MW-607M1_S26D	FD	03/24/2026	Ground Water	207.40	217.40
Central Impact Area	MW-323M1	MW-323M1_S26	N	03/23/2026	Ground Water	195.00	205.00
Central Impact Area	MW-699M1	MW-699M1_S26	N	03/23/2026	Ground Water	261.50	271.50
Central Impact Area	MW-616M1	MW-616M1_S26	N	03/23/2026	Ground Water	217.10	227.10
Central Impact Area	MW-625M2	MW-625M2_S26	MS	03/23/2026	Ground Water	230.00	240.00
Central Impact Area	MW-625M2	MW-625M2_S26	N	03/23/2026	Ground Water	230.00	240.00
Central Impact Area	MW-625M2	MW-625M2_S26	SD	03/23/2026	Ground Water	230.00	240.00
Central Impact Area	MW-625M1	MW-625M1_S26	N	03/23/2026	Ground Water	260.00	270.00
Central Impact Area	MW-626M1	MW-626M1_S26	N	03/19/2026	Ground Water	282.20	292.20
Central Impact Area	MW-149M1	MW-149M1_S26	N	03/19/2026	Ground Water	237.50	247.50
Central Impact Area	MW-42M3	MW-42M3_S26	N	03/19/2026	Ground Water	165.80	176.00
Central Impact Area	MW-42M2	MW-42M2_S26	N	03/19/2026	Ground Water	185.80	196.00

N = Normal Sample
FD = Field Duplicate

TABLE 1
Sampling Progress: March 2026

Area Of Concern	Location	Field Sample ID	Sample Type	Date Sampled	Matrix	Top of Screen (ft bgs)	Bottom of Screen (ft bgs)
Central Impact Area	MW-42M1	MW-42M1_S26	N	03/19/2026	Ground Water	205.80	216.00
Central Impact Area	MW-42M1	MW-42M1_S26D	FD	03/19/2026	Ground Water	205.80	216.00
Former A Range	MW-42M1	MW-42M1_S26	N	03/19/2026	Ground Water	205.80	216.00
Former A Range	MW-42M1	MW-42M1_S26D	FD	03/19/2026	Ground Water	205.80	216.00
Central Impact Area	MW-111M1	MW-111M1_S26	N	03/18/2026	Ground Water	224.00	234.00
Central Impact Area	MW-39M1	MW-39M1_S26	MS	03/18/2026	Ground Water	220.00	230.00
Central Impact Area	MW-39M1	MW-39M1_S26	N	03/18/2026	Ground Water	220.00	230.00
Central Impact Area	MW-39M1	MW-39M1_S26	SD	03/18/2026	Ground Water	220.00	230.00
Central Impact Area	MW-87M1	MW-87M1_S26	N	03/18/2026	Ground Water	194.00	204.00
Central Impact Area	MW-88M2	MW-88M2_S26	N	03/18/2026	Ground Water	213.00	223.00
Central Impact Area	MW-88M1	MW-88M1_S26	N	03/18/2026	Ground Water	233.00	243.00
Central Impact Area	MW-25	MW-25_S26	N	03/17/2026	Ground Water	108.00	118.00
Central Impact Area	MW-725M1	MW-725M1_S26	N	03/17/2026	Ground Water	145.20	155.20
Central Impact Area	MW-695S	MW-695S_S26	N	03/17/2026	Ground Water	130.00	140.00
Central Impact Area	MW-695S	MW-695S_S26D	FD	03/17/2026	Ground Water	130.00	140.00
Central Impact Area	MW-89M3	MW-89M3_S26	N	03/16/2026	Ground Water	174.00	184.00
Central Impact Area	MW-89M2	MW-89M2_S26	N	03/16/2026	Ground Water	214.00	224.00
Central Impact Area	MW-89M2	MW-89M2_S26D	FD	03/16/2026	Ground Water	214.00	224.00
Central Impact Area	MW-89M1	MW-89M1_S26	N	03/16/2026	Ground Water	234.00	244.00
Central Impact Area	MW-43M2	MW-43M2_S26	N	03/16/2026	Ground Water	200.00	210.00
Central Impact Area	MW-43M1	MW-43M1_S26	N	03/16/2026	Ground Water	223.00	233.00
Central Impact Area	MW-176M2	MW-176M2_S26	N	03/12/2026	Ground Water	229.00	239.00
Central Impact Area	MW-176M1	MW-176M1_S26	N	03/12/2026	Ground Water	270.00	280.00
Central Impact Area	MW-487M2	MW-487M2_S26	N	03/11/2026	Ground Water	195.84	205.84
J1 Range Northern	MW-487M2	MW-487M2_S26	N	03/11/2026	Ground Water	195.84	205.84
Central Impact Area	MW-487M1	MW-487M1_S26	N	03/11/2026	Ground Water	240.29	250.29
J1 Range Northern	MW-487M1	MW-487M1_S26	N	03/11/2026	Ground Water	240.29	250.29
J3 Range	J3-EFF	J3-EFF-234A	N	03/11/2026	Process Water	0.00	0.00

N = Normal Sample
FD = Field Duplicate

TABLE 1
Sampling Progress: March 2026

Area Of Concern	Location	Field Sample ID	Sample Type	Date Sampled	Matrix	Top of Screen (ft bgs)	Bottom of Screen (ft bgs)
J3 Range	J3-MID-2	J3-MID-2-234A	N	03/11/2026	Process Water	0.00	0.00
J3 Range	J3-MID-1	J3-MID-1-234A	N	03/11/2026	Process Water	0.00	0.00
J3 Range	J3-INF	J3-INF-234A	N	03/11/2026	Process Water	0.00	0.00
Central Impact Area	MW-59M2	MW-59M2_S26	N	03/11/2026	Ground Water	150.00	160.00
Central Impact Area	MW-59M1	MW-59M1_S26	N	03/11/2026	Ground Water	165.00	170.00
Demolition Area 1	D1-EFF	D1-EFF-188A	N	03/11/2026	Process Water	0.00	0.00
Demolition Area 1	D1-MID-2	D1-MID-2-188A	N	03/11/2026	Process Water	0.00	0.00
Demolition Area 1	D1-MID-1	D1-MID-1-188A	N	03/11/2026	Process Water	0.00	0.00
Demolition Area 1	D1-INF	D1-INF-188A	N	03/11/2026	Process Water	0.00	0.00
Central Impact Area	MW-107M2	MW-107M2_S26	N	03/11/2026	Ground Water	125.00	135.00
Central Impact Area	MW-37M2	MW-37M2_S26	MS	03/10/2026	Ground Water	145.00	155.00
Central Impact Area	MW-37M2	MW-37M2_S26	N	03/10/2026	Ground Water	145.00	155.00
Central Impact Area	MW-37M2	MW-37M2_S26	SD	03/10/2026	Ground Water	145.00	155.00
Central Impact Area	MW-486M1	MW-486M1_S26	MS	03/10/2026	Ground Water	185.70	195.70
Central Impact Area	MW-486M1	MW-486M1_S26	N	03/10/2026	Ground Water	185.70	195.70
Central Impact Area	MW-486M1	MW-486M1_S26	SD	03/10/2026	Ground Water	185.70	195.70
Central Impact Area	CIA2-EFF	CIA2-EFF-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA2-MID2	CIA2-MID2-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA2-MID1	CIA2-MID1-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA2-INF	CIA2-INF-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA1-EFF	CIA1-EFF-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA1-MID2	CIA1-MID2-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA1-MID1	CIA1-MID1-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA1-INF	CIA1-INF-146A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	MW-477M2	MW-477M2_S26	N	03/10/2026	Ground Water	145.62	155.62
Central Impact Area	MW-477M2	MW-477M2_S26D	FD	03/10/2026	Ground Water	145.62	155.62
Central Impact Area	CIA3-EFF	CIA3-EFF-117A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA3-MID2	CIA3-MID2-117A	N	03/10/2026	Process Water	0.00	0.00

N = Normal Sample
FD = Field Duplicate

TABLE 1
Sampling Progress: March 2026

Area Of Concern	Location	Field Sample ID	Sample Type	Date Sampled	Matrix	Top of Screen (ft bgs)	Bottom of Screen (ft bgs)
Central Impact Area	CIA3-MID1	CIA3-MID1-117A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	CIA3-INF	CIA3-INF-117A	N	03/10/2026	Process Water	0.00	0.00
Central Impact Area	MW-477M1	MW-477M1_S26	N	03/10/2026	Ground Water	187.53	197.53
Central Impact Area	MW-38M4	MW-38M4_S26	N	03/09/2026	Ground Water	132.00	142.00
Central Impact Area	MW-38M3	MW-38M3_S26	N	03/09/2026	Ground Water	170.00	180.00
Central Impact Area	MW-728M1	MW-728M1_S26	N	03/09/2026	Ground Water	153.40	163.40
J2 Range Northern	J2N-MID-2F	J2N-MID-2F-234A	N	03/09/2026	Process Water	0.00	0.00
J2 Range Northern	J2N-MID-1F	J2N-MID-1F-234A	N	03/09/2026	Process Water	0.00	0.00
J2 Range Northern	J2N-EFF-EF	J2N-EFF-EF-234A	N	03/09/2026	Process Water	0.00	0.00
J2 Range Northern	J2N-MID-2E	J2N-MID-2E-234A	N	03/09/2026	Process Water	0.00	0.00
J2 Range Northern	J2N-MID-1E	J2N-MID-1E-234A	N	03/09/2026	Process Water	0.00	0.00
J2 Range Northern	J2N-INF-EF	J2N-INF-EF-234A	N	03/09/2026	Process Water	0.00	0.00
J1 Range Northern	J1N-EFF	J1N-EFF-149A	N	03/09/2026	Process Water	0.00	0.00
Central Impact Area	MW-184M1	MW-184M1_S26	N	03/09/2026	Ground Water	186.00	196.00
J1 Range Northern	J1N-MID2	J1N-MID2-149A	N	03/09/2026	Process Water	0.00	0.00
J1 Range Northern	J1N-MID1	J1N-MID1-149A	N	03/09/2026	Process Water	0.00	0.00
J1 Range Northern	J1N-INF2	J1N-INF2-149A	N	03/09/2026	Process Water	0.00	0.00

N = Normal Sample
FD = Field Duplicate

TABLE 2
VALIDATED EXPLOSIVE AND PERCHLORATE RESULTS
Data Received 01 to 31 March 2026

Area of Concern	Location ID	Field Sample ID	Top Depth (ft bgs)	Bottom Depth (ft bgs)	Date Sampled	Test Method	Analyte	Result Value	Qualifier	Units	MCL/HA	> MCL/HA	MDL	RL
Central Impact Area	MW-485M1	MW-485M1_S26	125.32	135.32	02/19/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	2.6		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-485M1	MW-485M1_S26	125.32	135.32	02/19/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.57		µg/L	400		0.099	0.21
Central Impact Area	MW-485M1	MW-485M1_S26D	125.32	135.32	02/19/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	2.6		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-485M1	MW-485M1_S26D	125.32	135.32	02/19/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.58		µg/L	400		0.097	0.21
Central Impact Area	MW-40M1	MW-40M1_S26	132.50	142.00	02/18/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.17	J	µg/L	0.60		0.11	0.22
Central Impact Area	MW-729M1	MW-729M1_S26	231.50	241.50	02/18/2026	SW6850	Perchlorate	1.2		µg/L	2.0		0.10	0.20
Central Impact Area	MW-729M1	MW-729M1_S26	231.50	241.50	02/18/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	1.8		µg/L	0.60	X	0.11	0.22
Central Impact Area	MW-106M2	MW-106M2_S26	140.50	150.50	02/18/2026	SW8330B	2-Amino-4,6-dinitrotoluene	0.13	J	µg/L	7.3		0.052	1.1
Central Impact Area	MW-01S	MW-01S_S26	114.00	124.00	02/17/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.25		µg/L	0.60		0.11	0.22
Central Impact Area	MW-01S	MW-01S_S26	114.00	124.00	02/17/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.16	J	µg/L	400		0.099	0.22
Central Impact Area	MW-01M2	MW-01M2_S26	160.00	165.00	02/17/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	4.3		µg/L	0.60	X	0.11	0.22
Central Impact Area	MW-01M2	MW-01M2_S26	160.00	165.00	02/17/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.52		µg/L	400		0.10	0.22
Central Impact Area	MW-90S	MW-90S_S26	118.00	128.00	02/17/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.61		µg/L	0.60	X	0.11	0.22
Central Impact Area	MW-02M2	MW-02M2_S26	170.00	175.00	02/12/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.45		µg/L	0.60		0.12	0.24
Central Impact Area	OW-1	OW-1_S26	126.00	136.00	02/11/2026	SW8330B	1,3,5-Trinitrobenzene	0.13	J	µg/L	1090		0.048	0.21
Central Impact Area	OW-1	OW-1_S26	126.00	136.00	02/11/2026	SW8330B	2,4,6-Trinitrotoluene	2.8		µg/L	2.0	X	0.042	0.21
Central Impact Area	OW-1	OW-1_S26	126.00	136.00	02/11/2026	SW8330B	2,4-Dinitrotoluene	0.14	J	µg/L	5.0		0.059	0.21
Central Impact Area	OW-1	OW-1_S26	126.00	136.00	02/11/2026	SW8330B	2-Amino-4,6-dinitrotoluene	0.36	J	µg/L	7.3		0.052	1.1
Central Impact Area	OW-1	OW-1_S26	126.00	136.00	02/11/2026	SW8330B	4-Amino-2,6-dinitrotoluene	0.44		µg/L	7.3		0.063	0.21
Central Impact Area	OW-1	OW-1_S26	126.00	136.00	02/11/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.27	J	µg/L	0.60		0.10	0.21
Central Impact Area	OW-1	OW-1_S26D	126.00	136.00	02/11/2026	SW8330B	1,3,5-Trinitrobenzene	0.16	J	µg/L	1090		0.049	0.22
Central Impact Area	OW-1	OW-1_S26D	126.00	136.00	02/11/2026	SW8330B	2,4,6-Trinitrotoluene	2.8		µg/L	2.0	X	0.044	0.22
Central Impact Area	OW-1	OW-1_S26D	126.00	136.00	02/11/2026	SW8330B	2,4-Dinitrotoluene	0.11	J	µg/L	5.0		0.061	0.22
Central Impact Area	OW-1	OW-1_S26D	126.00	136.00	02/11/2026	SW8330B	2-Amino-4,6-dinitrotoluene	0.38	J	µg/L	7.3		0.053	1.1
Central Impact Area	OW-1	OW-1_S26D	126.00	136.00	02/11/2026	SW8330B	4-Amino-2,6-dinitrotoluene	0.46		µg/L	7.3		0.064	0.22
Central Impact Area	OW-1	OW-1_S26D	126.00	136.00	02/11/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.27	J	µg/L	0.60		0.11	0.22
Central Impact Area	MW-91S	MW-91S_S26	124.00	134.00	02/11/2026	SW8330B	1,3,5-Trinitrobenzene	0.19	J	µg/L	1090		0.047	0.21
Central Impact Area	MW-91S	MW-91S_S26	124.00	134.00	02/11/2026	SW8330B	2,4,6-Trinitrotoluene	1.5		µg/L	2.0		0.042	0.21

J = Estimated Result
MDL = Method Detection Limit
RL = Reporting Limit
ND = Non-Detect

MCL/HA= Either the MCL or Lowest Health Advisory Limit

TABLE 2
VALIDATED EXPLOSIVE AND PERCHLORATE RESULTS
Data Received 01 to 31 March 2026

Area of Concern	Location ID	Field Sample ID	Top Depth (ft bgs)	Bottom Depth (ft bgs)	Date Sampled	Test Method	Analyte	Result Value	Qualifier	Units	MCL/HA	> MCL/HA	MDL	RL
Central Impact Area	MW-91S	MW-91S_S26	124.00	134.00	02/11/2026	SW8330B	2-Amino-4,6-dinitrotoluene	0.16	J	µg/L	7.3		0.051	1.0
Central Impact Area	MW-91S	MW-91S_S26	124.00	134.00	02/11/2026	SW8330B	4-Amino-2,6-dinitrotoluene	0.14	J	µg/L	7.3		0.062	0.21
Central Impact Area	MW-91S	MW-91S_S26	124.00	134.00	02/11/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	1.3		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-91S	MW-91S_S26	124.00	134.00	02/11/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.11	J	µg/L	400		0.096	0.21
Central Impact Area	MW-91S	MW-91S_S26D	124.00	134.00	02/11/2026	SW8330B	1,3,5-Trinitrobenzene	0.22		µg/L	1090		0.047	0.21
Central Impact Area	MW-91S	MW-91S_S26D	124.00	134.00	02/11/2026	SW8330B	2,4,6-Trinitrotoluene	1.5		µg/L	2.0		0.042	0.21
Central Impact Area	MW-91S	MW-91S_S26D	124.00	134.00	02/11/2026	SW8330B	2-Amino-4,6-dinitrotoluene	0.17	J	µg/L	7.3		0.051	1.0
Central Impact Area	MW-91S	MW-91S_S26D	124.00	134.00	02/11/2026	SW8330B	4-Amino-2,6-dinitrotoluene	0.14	J	µg/L	7.3		0.062	0.21
Central Impact Area	MW-91S	MW-91S_S26D	124.00	134.00	02/11/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	1.4		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-91S	MW-91S_S26D	124.00	134.00	02/11/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.12	J	µg/L	400		0.096	0.21
Central Impact Area	MW-91M1	MW-91M1_S26	170.00	180.00	02/11/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	2.7		µg/L	0.60	X	0.11	0.21
Central Impact Area	MW-91M1	MW-91M1_S26	170.00	180.00	02/11/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.25		µg/L	400		0.099	0.21
Central Impact Area	MW-93M2	MW-93M2_S26	145.00	155.00	02/10/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	0.68		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-101M1	MW-101M1_S26	158.00	168.00	02/10/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	5.4		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-101M1	MW-101M1_S26	158.00	168.00	02/10/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.46		µg/L	400		0.097	0.21
Central Impact Area	MW-101M1	MW-101M1_S26D	158.00	168.00	02/10/2026	SW8330B	Hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX)	5.4		µg/L	0.60	X	0.10	0.21
Central Impact Area	MW-101M1	MW-101M1_S26D	158.00	168.00	02/10/2026	SW8330B	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	0.50		µg/L	400		0.098	0.21

J = Estimated Result
MDL = Method Detection Limit
RL = Reporting Limit
ND = Non-Detect

MCL/HA= Either the MCL or Lowest Health Advisory Limit